

PARAMETRIC ESTIMATION OF THE PROCESS CAPABILITY INDEX S''_{pk} AND ITS APPLICATION TO ELECTRONIC INDUSTRIES

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Abstract

The proposed index is the process capability index used in the electronics industries to measure the capability of the process. This article focuses on process capability index, specifically applicable to normal random variables. The article has three main objectives: Firstly, we explore various classical estimation methods for the proposed index from frequentist approaches for normal distributions and compare their performance based on mean squared errors. Second, we calculate the classical confidence interval for the proposed index, which includes the asymptotic confidence interval. Third, we examine both Bayes point and interval estimation under symmetric and asymmetric loss functions for the proposed index. A Monte Carlo and Markov Chain Monte Carlo simulation study is conducted to compare the performance of the classical and the Bayes estimates of the proposed index for some set of parameters. Finally, to demonstrate the applicability of this index, two real data sets from the electronics industry are re-analyzed.

Keywords: Asymptotic confidence interval, Bayesian estimation, classical methods of estimation, point and interval estimation.

Abbreviations and notations

ACI	: Asymptotic confidence interval.
AW	: Average width.
BE	: Bayes estimate.
CI	: Confidence interval.
CP	: Coverage probability.
CME	: Cramér-von-Mises estimator.
CDF	: Cumulative distribution function.
HPD	: Highest posterior density.
IG	: Inverse gamma.
KLF	: K-loss function.
LSE	: Least squares estimator.
LINEX	: Linear exponential.
LSLF	: Logarithmic squared error loss function.
MCMC	: Markov Chain Monte Carlo.
MLE	: Maximum likelihood estimator.
MPSIE	: Maximum product of spacing estimator.
MSE	: Mean squared error.
MSELF	: Modified squared error loss function.
MC	: Monte Carlo.
NLM	: Non-linear minimization.
PE	: Percentile estimator.
PR	: Posterior risk.
PDF	: Probability density function.
PCI	: Process capability index.
SELF	: Squared error loss function.
WLSIE	: Weighted least square estimator.
WSELF	: Weighted squared error loss function.

1. INTRODUCTION

Across all manufacturing sectors, processes are routinely evaluated to determine their capacity using various instruments and methods to verify whether a process under observation meets a given set of requirements or standards. PCI is the tool of choice for manufacturers because it has been proven to help with decision-making and improve process performance. PCIs have garnered significant attention, particularly in the field of quality assurance. When studying traditional capability indices, it is often assumed that with a process mean κ and process standard deviation ζ a normal probability model is used. This assumption has contributed to the widespread interest in PCIs, particularly in quality assurance. For a deeper understanding of various capability indices, readers may refer to: C_p Juran, Gryna and Bingham [11], C_{pk} Kane [12], C_{pm} Chang, Cheng and Spiring [4]; Hsiang and Taguchi [10], C_{pmk} Pearn, Kotz and Jhonson [15]; Wu and Pearn [27], $C_p(u, v)$ Vannman [25], S_{pk} Boyles [1]; Chen and Pearn [2]; Saha [17] and many others. The Boyles [1] PCI, S_{pk} was defined as

$$S_{pk} = \frac{1}{3} \Phi^{-1} \left\{ \frac{1}{2} \Phi \left(\frac{U - \kappa}{\zeta} \right) + \frac{1}{2} \Phi \left(\frac{\kappa - L}{\zeta} \right) \right\} \quad (1)$$

here, U and L represent the upper and lower specification limits, respectively, and $\Phi(\cdot)$ is the CDF of $N(0, 1)$ and defined as:

$$F(y|\kappa, \zeta) = \Phi \left(\frac{y - \kappa}{\zeta} \right) ; y, \kappa \in \mathcal{R}, \zeta > 0 \quad (2)$$

with the PDF of normal distribution,

$$f(y|\kappa, \zeta) = \frac{1}{\zeta\sqrt{2\pi}} e^{-\frac{1}{2}\left(\frac{y-\kappa}{\zeta}\right)^2}; \quad y, \kappa \in \mathcal{R}, \zeta > 0. \quad (3)$$

One of the drawbacks of S_{pk} is that it ignores the target value of the process. Its inability to represent a situation in which the process is not centred on the target value is another disadvantage. To address this problem, a new index was created that considers deviations from the desired value when determining a process's capabilities. In the article by Saha [17], using SELF a capability index, a measure designed to assess the performance of a process relative to its specification limits. This index was subsequently cited and discussed by Saha, Devi and Pareek [18], while its inferential properties were rigorously investigated by Saha et al. [19]. Building upon this prior foundation, the present study develops a novel asymmetric loss-based process capability index, denoted as S''_{pk} , specifically for processes that can be modeled by a normal distribution.

The proposed index is formulated by incorporating the LINEX loss function by Varia [26], as a tool for decision-making under asymmetric loss conditions. This loss function has proven useful in various statistical inference settings where the cost of overestimation and underestimation differ. In process capability analysis, Saha and Dey [21] have previously applied the LINEX loss to address such asymmetries, making it a natural choice for the development of S''_{pk} . Mathematically, the LINEX loss function is expressed as: $L_2(\kappa - T) = 2 \frac{e^{\omega(\kappa - T)} - \omega(\kappa - T) - 1}{\omega^2}$, where ω is a fixed parameter that controls the degree of asymmetry of L_2 . For small values of ω (e.g., $\omega = 0.01$), this loss function becomes nearly symmetric and resembles the quadratic loss function, $L(\kappa - T) = (\kappa - T)^2$ Erfanian and Gildeh [9].

The index S''_{pk} , as developed by Dey, Saha and Park [7] and further refined by Saha and Dey [20] is obtained by incorporating the LINEX loss function into the denominator of the conventional S_{pk} PCI. This modification results in a capability measure that directly accounts for asymmetric loss considerations in evaluating process performance, and is given by

$$S''_{pk} = \frac{1}{3} \Phi^{-1} \left\{ \frac{1}{2} \Phi \left(\frac{U - \kappa}{\sqrt{\zeta^2 + 2 \frac{e^{\omega(\kappa - T)} - \omega(\kappa - T) - 1}{\omega^2}}} \right) + \frac{1}{2} \Phi \left(\frac{\kappa - L}{\sqrt{\zeta^2 + 2 \frac{e^{\omega(\kappa - T)} - \omega(\kappa - T) - 1}{\omega^2}}} \right) \right\} \quad (4)$$

The term $2 \frac{e^{\omega(\kappa - T)} - \omega(\kappa - T) - 1}{\omega^2}$ captures two types of variation: (i) is within-process variation, which reflects the natural variability of individual observation around the process mean κ , (ii) between-process deviation, which represents the departure of the process mean κ from the desired target value T . Together, both the inherent dispersion of the process and its alignment with the target specifications.

The primary objective of this study is to examine the performance characteristics of six well-known frequentist estimation methods previously employed by Dey et al. [8]. These estimators include the MLE, LSE, WLSE, PE, CME and MPSE. We focuses on their application to the S''_{pk} under various combinations of sample sizes and parameter settings. The evaluation criterion for these estimators is their MSEs, which balances both bias and variability in estimation. Since the theoretical comparison of these estimators is analytically intractable owing to the complex form of S''_{pk} and the absence of closed form variance expression, a comprehensive simulation study is undertaken. The primary focus is on the MLE, given its widespread use and desirable asymptotic properties. The second objective is the study is to derive an ACI for S''_{pk} .

To assess the performance of the interval, the AW and CP are calculated. The third objective is to obtain the Bayesian point and interval estimates for S''_{pk} . The novelty of this study lies in the fact that, to date, there have been no reports on the estimation of S''_{pk} or the construction of ACI using the MLE method. Thus, this study aims to provide applied statisticians and quality control engineers with guidance on selecting the optimal estimation method among the six distinct frequentist approaches. To assess interval quality, both AW and CP are computed. The

third objective is to develop Bayesian point and interval estimates for S''_{pk} , offering a probabilistic alternative to the frequentist framework. The novelty of this work lies in the fact that, to the best of our knowledge, no prior research has addressed the estimation of S''_{pk} or the construction of \mathcal{ACI} for it using MLE approach.

Rest of the article is structured as follows. In Section 2, the estimation methods for S''_{pk} are introduced, and the corresponding estimators are derived. This section also includes the construction of \mathcal{ACI} for S''_{pk} based on the MLE, as well as Bayesian estimation using five different loss functions. Section 3 presents a comprehensive MC and MCMC simulation study to compare the performances of S''_{pk} based on the various estimation methods. In Section 4, two real datasets from the electronics industry are analyzed for illustration. Finally, Section 5 provides the concluding remarks.

2. ESTIMATION OF THE INDEX S''_{pk}

This section investigates the point and interval estimation of the index S''_{pk} from classical and Bayesian point of view, respectively.

2.1. Classical estimation

A random variable Y has $N(\kappa, \zeta)$, with its CDF, given in equation (2) and PDF, given in equation (3) where κ, ζ are the parameters of the distribution and $\Phi(\cdot)$ is the CDF of the standard normal variate. In the context of the considered model, the analytical forms of the derivatives and necessary transformations are not available in closed form for the parameter estimation procedures. Consequently, for all the considered estimation methods the parameter estimates were obtained using the NLM technique. A short formulation of the considered classical methods of estimation are provided in brief in Table 1, followed by the final expression for the derived PCI based on the estimated values of the parameters. Note that only the method of MLE and MPSE satisfied the invariance property and hence we got the MLE and MPSE of the index S''_{pk} by using the invariance property and for the remaining considered methods we have used the plug-in method to obtain the estimate of the index. The detailed description of these methods of estimation in the context of process capability analysis the readers may refer to the articles Saha, Devi and Pareek [18], Saha et al. [19], Saha and Dey [21] and many more.

Asymptotic confidence interval

\mathcal{ACI} of S''_{pk} in case of normal distribution, can be derived with $100(1 - \omega)\%$ CI. \mathcal{ACI} of S''_{pk} can be obtained as:

$$\frac{\hat{S}''_{pk} - S''_{pk}}{\sqrt{\text{var}(\hat{S}''_{pk})}} \sim N(0, 1)$$

where,

$$\begin{aligned} \text{var}(\hat{S}''_{pk}) = & \left(\frac{\partial S''_{pk}}{\partial \kappa} \right)^2 \times \left(-\frac{1}{E \left(\frac{\partial^2 \ln L(\kappa, \zeta)}{\partial \kappa^2} \right)} \right) + \left(\frac{\partial S''_{pk}}{\partial \zeta} \right)^2 \times \left(-\frac{1}{E \left(\frac{\partial^2 \ln L(\kappa, \zeta)}{\partial \zeta^2} \right)} \right) \\ & - 2 \left(\frac{\partial S''_{pk}}{\partial \kappa} \right) \left(\frac{\partial S''_{pk}}{\partial \zeta} \right) \times \left(-\frac{1}{E \left(\frac{\partial^2 \ln L(\kappa, \zeta)}{\partial \kappa \partial \zeta} \right)} \right). \end{aligned}$$

The elements of Fisher information matrix

$$I(\theta) = E \left\{ \begin{pmatrix} \frac{\partial^2 \ln L(\kappa, \zeta)}{\partial \kappa^2} & \frac{\partial^2 \ln L(\kappa, \zeta)}{\partial \kappa \partial \zeta} \\ \frac{\partial^2 \ln L(\kappa, \zeta)}{\partial \zeta \partial \kappa} & \frac{\partial^2 \ln L(\kappa, \zeta)}{\partial \zeta^2} \end{pmatrix} \right\}$$

Table 1: Classical methods of estimation and corresponding estimated PCI

Method	Function to be optimized	Expression of estimated index S''_{pk}
MLE	$\log \left(\left(\frac{1}{2\pi\zeta^2} \right)^{\frac{n}{2}} e^{-\frac{1}{2} \sum_{i=1}^n \left(\frac{y_i - \kappa}{\zeta} \right)^2} \right)$	$\frac{1}{3} \Phi^{-1} \left\{ \frac{1}{2} \Phi \left(\frac{U - \hat{\kappa}_{mle}}{\sqrt{\zeta_{mle}^2 + \frac{2(e^{\omega(\hat{\kappa}_{mle} - T)} - \omega(\hat{\kappa}_{mle} - T) - 1)}{\omega^2}}}} \right) + \frac{1}{2} \Phi \left(\frac{\hat{\kappa}_{mle} - L}{\sqrt{\zeta_{mle}^2 + \frac{2(e^{\omega(\hat{\kappa}_{mle} - T)} - \omega(\hat{\kappa}_{mle} - T) - 1)}{\omega^2}}} \right) \right\}$
LSE	$\sum_{i=1}^n \left\{ F(y_{(i:n)} \kappa, \zeta) - \frac{i}{n+1} \right\}^2$	$\frac{1}{3} \Phi^{-1} \left\{ \frac{1}{2} \Phi \left(\frac{U - \hat{\kappa}_{lse}}{\sqrt{\zeta_{lse}^2 + \frac{2(e^{\omega(\hat{\kappa}_{lse} - T)} - \omega(\hat{\kappa}_{lse} - T) - 1)}{\omega^2}}} \right) + \frac{1}{2} \Phi \left(\frac{\hat{\kappa}_{lse} - L}{\sqrt{\zeta_{lse}^2 + \frac{2(e^{\omega(\hat{\kappa}_{lse} - T)} - \omega(\hat{\kappa}_{lse} - T) - 1)}{\omega^2}}} \right) \right\}$
WLSE	$\sum_{i=1}^n w_i \left\{ F(y_{(i:n)} \kappa, \zeta) - \frac{i}{n+1} \right\}^2$	$\frac{1}{3} \Phi^{-1} \left\{ \frac{1}{2} \Phi \left(\frac{U - \hat{\kappa}_{wlse}}{\sqrt{\zeta_{wlse}^2 + \frac{2(e^{\omega(\hat{\kappa}_{wlse} - T)} - \omega(\hat{\kappa}_{wlse} - T) - 1)}{\omega^2}}} \right) + \frac{1}{2} \Phi \left(\frac{\hat{\kappa}_{wlse} - L}{\sqrt{\zeta_{wlse}^2 + \frac{2(e^{\omega(\hat{\kappa}_{wlse} - T)} - \omega(\hat{\kappa}_{wlse} - T) - 1)}{\omega^2}}} \right) \right\}$
PIE	$\sum_{j=1}^n \left\{ y_{(i:n)} - Q(p_i \kappa, \zeta) \right\}^2$	$\frac{1}{3} \Phi^{-1} \left\{ \frac{1}{2} \Phi \left(\frac{U - \hat{\kappa}_{pe}}{\sqrt{\zeta_{pe}^2 + \frac{2(e^{\omega(\hat{\kappa}_{pe} - T)} - \omega(\hat{\kappa}_{pe} - T) - 1)}{\omega^2}}} \right) + \frac{1}{2} \Phi \left(\frac{\hat{\kappa}_{pe} - L}{\sqrt{\zeta_{pe}^2 + \frac{2(e^{\omega(\hat{\kappa}_{pe} - T)} - \omega(\hat{\kappa}_{pe} - T) - 1)}{\omega^2}}} \right) \right\}$
CME	$\frac{1}{12n} + \sum_{i=1}^n \left\{ F(y_{(i:n)} \kappa, \zeta) - \frac{2i-1}{2n} \right\}^2$	$\frac{1}{3} \Phi^{-1} \left\{ \frac{1}{2} \Phi \left(\frac{U - \hat{\kappa}_{cme}}{\sqrt{\zeta_{cme}^2 + \frac{2(e^{\omega(\hat{\kappa}_{cme} - T)} - \omega(\hat{\kappa}_{cme} - T) - 1)}{\omega^2}}} \right) + \frac{1}{2} \Phi \left(\frac{\hat{\kappa}_{cme} - L}{\sqrt{\zeta_{cme}^2 + \frac{2(e^{\omega(\hat{\kappa}_{cme} - T)} - \omega(\hat{\kappa}_{cme} - T) - 1)}{\omega^2}}} \right) \right\}$
MPSIE	$\frac{1}{(n+1)} \sum_{i=1}^{n+1} \log \left(F(y_{(i:n)} \kappa, \zeta) \right) - F(y_{(i-1:n)} \kappa, \zeta)$	$\frac{1}{3} \Phi^{-1} \left\{ \frac{1}{2} \Phi \left(\frac{U - \hat{\kappa}_{mpse}}{\sqrt{\zeta_{mpse}^2 + \frac{2(e^{\omega(\hat{\kappa}_{mpse} - T)} - \omega(\hat{\kappa}_{mpse} - T) - 1)}{\omega^2}}} \right) + \frac{1}{2} \Phi \left(\frac{\hat{\kappa}_{mpse} - L}{\sqrt{\zeta_{mpse}^2 + \frac{2(e^{\omega(\hat{\kappa}_{mpse} - T)} - \omega(\hat{\kappa}_{mpse} - T) - 1)}{\omega^2}}} \right) \right\}$

can easily be obtained, where

$$E\left(\frac{\partial^2 \ln L(\kappa, \zeta)}{\partial \kappa^2}\right) = -\frac{n}{\zeta^2}, E\left(\frac{\partial^2 \ln L(\kappa, \zeta)}{\partial \zeta^2}\right) = -\frac{2n}{\zeta^2} \text{ and } E\left(\frac{\partial^2 \ln L(\kappa, \zeta)}{\partial^2 \kappa^2 \zeta^2}\right) = 0$$

After, obtaining partial derivative of S''_{pk} with respect to κ and ζ . Using, $(\Phi^{-1})'(y) = \frac{1}{\Phi'(\Phi^{-1}(y))}$, with $\Phi' (= \phi)$ as the first derivative of Φ . We get it as:

$$\begin{aligned} \frac{\partial S''_{pk}}{\partial \kappa} &= \frac{1}{6} \frac{1}{\Phi'(3S''_{pk})} \times \left\{ \phi\left(\frac{\mathbf{U} - \kappa}{\sqrt{\zeta^2 + 2\frac{e^{\omega(\kappa - \mathbf{T})} - \omega(\kappa - \mathbf{T}) - 1}}{\omega^2}}}\right) \right. \\ &\quad \left(-\frac{1}{\sqrt{\left(\zeta^2 + 2\frac{e^{\omega(\kappa - \mathbf{T})} - \omega(\kappa - \mathbf{T}) - 1}}{\omega^2}\right)}} - \frac{(\mathbf{U} - \kappa)(e^{\omega(\kappa - \mathbf{T})} - 1)}{\omega\left(\zeta^2 + 2\frac{e^{\omega(\kappa - \mathbf{T})} - \omega(\kappa - \mathbf{T}) - 1}}{\omega^2}\right)^{3/2}} \right) \\ &\quad + \phi\left(\frac{\kappa - \mathbf{L}}{\sqrt{\zeta^2 + 2\frac{e^{\omega(\kappa - \mathbf{T})} - \omega(\kappa - \mathbf{T}) - 1}}{\omega^2}}}\right) \\ &\quad \left. \left(\frac{1}{\sqrt{\left(\zeta^2 + 2\frac{e^{\omega(\kappa - \mathbf{T})} - \omega(\kappa - \mathbf{T}) - 1}}{\omega^2}\right)}} - \frac{(\kappa - \mathbf{L})(e^{\omega(\kappa - \mathbf{T})} - 1)}{\omega\left(\zeta^2 + 2\frac{e^{\omega(\kappa - \mathbf{T})} - \omega(\kappa - \mathbf{T}) - 1}}{\omega^2}\right)^{3/2}} \right) \right\} \\ \frac{\partial S''_{pk}}{\partial \zeta} &= \frac{1}{6} \frac{1}{\Phi'(3S''_{pk})} \times \left\{ \phi\left(\frac{\mathbf{U} - \kappa}{\sqrt{\zeta^2 + 2\frac{e^{\omega(\kappa - \mathbf{T})} - \omega(\kappa - \mathbf{T}) - 1}}{\omega^2}}}\right) \right. \\ &\quad \left(\frac{-(\mathbf{U} - \kappa)\zeta}{\left(\zeta^2 + 2\frac{e^{\omega(\kappa - \mathbf{T})} - \omega(\kappa - \mathbf{T}) - 1}}{\omega^2}\right)^{3/2}} \right) + \phi\left(\frac{\kappa - \mathbf{L}}{\sqrt{\zeta^2 + 2\frac{e^{\omega(\kappa - \mathbf{T})} - \omega(\kappa - \mathbf{T}) - 1}}{\omega^2}}}\right) \\ &\quad \left. \left(\frac{-(\kappa - \mathbf{L})\zeta}{\left(\zeta^2 + 2\frac{e^{\omega(\kappa - \mathbf{T})} - \omega(\kappa - \mathbf{T}) - 1}}{\omega^2}\right)^{3/2}} \right) \right\} \end{aligned}$$

Hence, the $(1 - \omega)100\%$ AIC of S''_{pk} can be obtained as:

$$\left\{ \left(\hat{S}'_{pk} - \mathbf{Z}_{(\frac{\omega}{2})} \sqrt{\text{var}(\hat{S}'_{pk})} \right), \left(\hat{S}'_{pk} + \mathbf{Z}_{(\frac{\omega}{2})} \sqrt{\text{var}(\hat{S}'_{pk})} \right) \right\}$$

where, $\mathbf{Z}_{(\omega/2)}$ is upper $(\omega/2)^{th}$ quantile of the $N(0, 1)$.

2.2. Bayesian estimation

This section focuses on the Bayesian estimation of the newly developed index S''_{pk} . In Bayesian theory, the accuracy of estimation depends on the careful selection of the prior distribution and loss function. The prior reflects initial beliefs about the parameters, while the loss function quantifies estimation errors. Both choices are essential for guiding the posterior distribution towards an accurate estimate. The importance of these components is highlighted by Shiau, Chiang and Hung [22], Spiring et al. [23], and Dey and Saha [6], who demonstrate how the appropriate selection of prior and loss function can enhance the robustness and efficiency of Bayesian estimation. The IPDF of the considered prior for the parameters κ and $\zeta^2 = \tau$ are given by

$$\pi_1(\kappa|\tau) = \frac{1}{\sqrt{2\pi\tau}} e^{-\frac{1}{2\tau}(\kappa - \kappa_0)^2}, \quad \kappa, \kappa_0 \in R, \tau > 0. \tag{5}$$

$$\pi_2(\tau) = \frac{\beta^\alpha}{\omega(\alpha)} \tau^{-(\alpha+1)} e^{-\frac{\beta}{\tau}}, \quad \alpha, \beta, \tau > 0. \tag{6}$$

where, the hyper-parameters α , β , and κ_0 are assumed to be known. Hence, the joint prior density function of κ and τ can be written as

$$\pi(\kappa, \tau) = \frac{1}{\sqrt{2\pi\tau}} \frac{\beta^\alpha}{\omega(\alpha)} e^{-\frac{1}{2\tau}(\kappa-\kappa_0)^2 - \frac{\beta}{\tau}} \tau^{-(\alpha+1)} \tag{7}$$

The joint posterior distribution is obtained by combining the likelihood function and prior distribution, and it is given by;

$$p(\kappa, \tau|y) \propto (\tau)^{-\frac{(n+3)}{2} - \alpha} e^{-\frac{1}{2\tau}\{S_{kk} + (n+1)(\kappa-\kappa_1)^2\}} \tag{8}$$

where, $\kappa_1 = \frac{n\bar{y} + \kappa_0}{n+1}$ and $S_{kk} = S_y + 2\beta + \frac{n(\kappa_0 - \bar{y})^2}{n+1}$. The marginal posterior distributions of the parameter τ and κ given y are in the following equations;

$$\pi(\tau|y) \propto \tau^{-\left(\frac{n}{2} + \alpha + 1\right)} e^{-\left(\frac{1}{\tau} \left(\frac{S_{kk}}{2}\right)\right)} \tag{9}$$

$$\pi(\kappa|y) \propto \frac{1}{\sqrt{\pi}} \frac{\omega\left(\frac{n+1+2\alpha}{2}\right)}{\omega(n+2\alpha)} \frac{\sqrt{(n+1)}}{\sqrt{S_{kk}}} \left\{1 + \frac{(\kappa - \kappa_1)^2}{S_{kk}/(n+1)}\right\}^{-\left(\frac{n+1+2\alpha}{2}\right)} \tag{10}$$

respectively. The Eqn. (9) is the marginal posterior distribution of τ which represents inverse gamma distribution, i.e., $\tau \sim \text{IG}\left(\frac{n+2\alpha}{2}, \frac{S_{kk}}{2}\right)$. In Eqn. (10), shows the marginal posterior distribution of κ which is unknown distribution. However, $\sqrt{N} \left(\frac{\kappa - \kappa_1}{\sqrt{S_{kk}/(n+1)}}\right)$ follows a t-distribution with $N = n + 2\alpha$ degrees of freedom. Since the joint posterior distribution does not have a closed-form expression, the marginal posterior distributions will be used to generate posterior random deviates through the MCMC algorithm. Using the marginal posterior distributions of κ and τ , the BE of the index S''_{pk} is obtained by generating MCMC random deviates. This is done using five different loss functions: SELF, WSELF, MSELF, LSLF, and KLF. The expressions of the loss functions, the associated BE and PR are given in tabular form in the following Table 2.

Table 2: BE and PR under different loss functions.

Name of the loss function	Form of the loss function	Bayes estimates	Posterior risk
SELF	$(\theta - d)^2$	$E(\theta X)$	$V(\theta X)$
WSELF	$\frac{(\theta-d)^2}{\theta}$	$(E(\theta^{-1} X))^{-1}$	$E(\theta X) - (E(\theta^{-1} X))^{-1}$
MSELF	$\left(1 - \frac{d}{\theta}\right)^2$	$\frac{E(\theta^{-1} X)}{E(\theta^{-2} X)}$	$1 - \frac{E(\theta^{-1} X)^2}{E(\theta^{-2} X)}$
LLF	$(\log \theta - \log d)^2$	$\exp(E(\log \theta X))$	$Var(\log \theta X)$
KLF	$\left(\sqrt{\frac{d}{\theta}} - \sqrt{\frac{\theta}{d}}\right)$	$\sqrt{\frac{E(\theta X)}{E(\theta^{-1} X)}}$	$E\{E(\theta X)(E(\theta^{-1} X)) - 1\}$

The following steps have been utilized in order to obtain posterior samples from the respective marginal distributions.

- Step-1:** Set preliminary estimate value $(\tau^{(0)}, \kappa^{(0)})$
- Step-2:** To start with $p = 1$.
- Step-3:** Generate a new sampler for τ and κ as follows: $\tau^{(p)} \sim \pi(y|\tau^{(p-1)})$, $\kappa^{(p)} \sim \pi(y|\kappa^{(p)})$
- Step-4:** We obtain the posterior samples of size \mathbb{P} for parameters τ and κ . After repeating the

step 2 and step 3 for $r = 1, 2, 3, \dots, \mathbb{P} (= 10000)$ times.

Step-5: We get a sequence $S''_{pk}^{(p)}$ by using the step-4 in above sequence.

Step-6: After receiving the posterior samples, the corresponding BE of S''_{pk} can be obtained from the above MCMC algorithm based on the above defined loss functions.

Step-7: The Bayes credible interval for the proposed index S''_{pk} is constructed by utilizing the sequences of random deviates $S''_{pk}^{(p)}$, $r = 1, 2, 3, \dots, \mathbb{P}$ obtained through step 5. Using, algorithm the $(1 - \omega)100\%$ highest posterior density credible interval of the index is given by, $\{S''_{pk}^{(p_1^*)}, S''_{pk}^{(p_1^* + (1-\delta)\mathbb{P})}\}$, where, (p_1^*) satisfying,

$$S''_{pk}^{(p_1^* + (1-\delta)\mathbb{P})} - S''_{pk}^{(p_1^*)} = \min \left(S''_{pk}^{(p_1 + (1-\delta)\mathbb{P})} - S''_{pk}^{(p_1)} \right)$$

3. SIMULATION AND DISCUSSION

This section employs MC simulations to evaluate the performances of the PCI S''_{pk} across different estimation methods by analyzing their MSEs and simulated risks. Additionally, the AWs and CIPs of the ACI is evaluated to measure the performance. The simulation study examines sample sizes $n = 20, 30, 50, 100$ and values of $\omega = 0.01, 1, 5, 10$, with several sets of parameter values: $(\kappa, \zeta) = (6.5, 1.25), (6.5, 1.50), (6.5, 1.75), (7.5, 1.25), (7.5, 1.50), (7.5, 1.75)$. The lower, target and upper specification limits are set at 0.50, 7.0, and 12.50, respectively.

In Tables 3 and 4, the values of S''_{pk} along with the average estimates and MSEs for each estimation method, are presented. The results of the ACI using MLE as the estimation method for S''_{pk} is shown in Table 5, with various values of ω . The finding from tables reveals that, among all the estimation methods, MLE yields the best performance in terms of MSEs. Furthermore, the MSEs decreases, with increase in sample size, demonstrating the consistency of the estimators. Additionally, as κ increases, the true value of S''_{pk} also increases. The analysis incorporated AWs and CIPs by using MLE, as the method of estimation for the ACI of S''_{pk} , because MLE is performing better among all other estimation methods. The findings also indicate that as sample size increases AW decrease and CIP increases. Next, the Bayes point and interval estimation for the index have been considered under the above mentioned priors using symmetric and asymmetric loss functions. The BE and IPR along with coverage probability (CIP) and average width (AW) are calculated for the considered setup, and presented in Tables 6 and 7 for four different values of ω . The values of hyper-parameters in Bayesian setup are chosen as $\alpha = 1.55$, $\beta = 0.05$ and $\kappa_0 = 5$ so that it coincides with the parameter value with smallest variation in the simulation study. The simulation study suggests that with the increase in sample size posterior risk decreases for all setups. Also as further, the CIPs increases and tend to the nominal value and their AWs decreases with increase in sample size. Moreover, the IPR is decreases for small values of ω and increase for large values of ω . As ω value increase from 0.01 to 5, IPR decreases and for $\omega = 10$, IPR increases.

Table 3: Estimates and MSE for $\omega = (0.01, 1)$ using MLE, LSE, WLSE, FE, CME, and MPSE with S'_{pk} .

PCI	MLE			LSE			WLSE			FE			CME			MPSE				
	Parameters	S'_{pk}	n	MLE	MSE	LSE	MSE	WLSE	MSE	FE	MSE	FE	MSE	CME	MSE	CME	MSE	MPSE	MSE	
$\omega = 0.01$	$S'_{pk}=1.48556$ $k=6.5$ $\zeta=1.25$	20	1.50973	0.05563	1.3974	0.07406	1.37641	0.08297	1.38714	0.08044	1.52055	0.07949	1.66466	1.52055	0.07949	1.66466	1.52055	0.07949	1.66466	0.10776
		30	1.51405	0.04007	1.43546	0.05086	1.40451	0.0629	1.41229	0.0617	1.54164	0.06193	1.62528	1.54164	0.06193	1.62528	1.54164	0.06193	1.62528	0.07026
		50	1.49475	0.0227	1.44589	0.02983	1.40113	0.04624	1.40921	0.04446	1.53128	0.0375	1.5689	1.53128	0.0375	1.5689	1.53128	0.0375	1.5689	0.0336
	100	1.48988	0.01182	1.48061	0.01616	1.41013	0.03225	1.4181	0.03225	1.4181	0.03406	1.54252	1.4181	0.03406	1.54252	1.4181	0.03406	1.54252	0.01525	
	$S'_{pk}=1.26491$ $k=6.5$ $\zeta=1.50$	20	1.28681	0.04183	1.19082	0.0539	1.16949	0.05955	1.18102	0.05966	1.29558	0.0606	1.42174	1.29558	0.0606	1.42174	1.29558	0.0606	1.42174	0.08114
		30	1.28335	0.02826	1.21746	0.03671	1.18246	0.0496	1.1895	0.04881	1.31155	0.0448	1.38185	1.31155	0.0448	1.38185	1.31155	0.0448	1.38185	0.04938
		50	1.28028	0.01731	1.24824	0.02223	1.20778	0.03866	1.20389	0.03476	1.32169	0.03135	1.34511	1.32169	0.03135	1.34511	1.32169	0.03135	1.34511	0.02632
	100	1.26432	0.00764	1.25798	0.01245	1.1987	0.02871	1.20185	0.02716	1.31211	0.0193	1.3031	1.31211	0.0193	1.3031	1.31211	0.0193	1.3031	0.01003	
	$S'_{pk}=1.09888$ $k=6.5$ $\zeta=1.75$	20	1.1113	0.03166	1.03214	0.04193	1.00968	0.05134	1.01655	0.04934	1.12731	0.0481	1.22943	1.12731	0.0481	1.22943	1.12731	0.0481	1.22943	0.06043
30		1.1044	0.01984	1.05015	0.02608	1.01985	0.03932	1.02446	0.0359	1.13177	0.03145	1.19013	1.13177	0.03145	1.19013	1.13177	0.03145	1.19013	0.03351	
50		1.0313	0.01201	1.07601	0.01617	1.03992	0.03052	1.03577	0.02639	1.14655	0.02235	1.1598	1.14655	0.02235	1.1598	1.14655	0.02235	1.1598	0.01763	
100	1.09833	0.00623	1.09709	0.00949	1.05642	0.03173	1.04423	0.02139	1.14586	0.01383	1.13279	1.14586	0.01383	1.13279	1.14586	0.01383	1.13279	0.00797		
$S'_{pk}=1.29514$ $k=7.5$ $\zeta=1.25$	20	1.35925	0.06525	1.2459	0.08371	1.23488	0.08935	1.23673	0.09022	1.41289	0.0125	1.48825	1.41289	0.0125	1.48825	1.41289	0.0125	1.48825	0.1236	
	30	1.32959	0.03824	1.24445	0.0572	1.21999	0.06755	1.22185	0.0695	1.39272	0.0819	1.42258	1.39272	0.0819	1.42258	1.39272	0.0819	1.42258	0.06284	
	50	1.31198	0.02261	1.26614	0.03401	1.2263	0.04865	1.22865	0.03807	1.38202	0.0587	1.37209	1.38202	0.0587	1.37209	1.38202	0.0587	1.37209	0.03213	
100	1.30772	0.01199	1.3012	0.02075	1.239	0.03641	1.23851	0.03764	1.38477	0.03764	1.34297	1.38477	0.03764	1.34297	1.38477	0.03764	1.34297	0.01544		
$S'_{pk}=1.11905$ $k=7.5$ $\zeta=1.50$	20	1.16814	0.04617	1.06321	0.06068	1.05601	0.07508	1.05235	0.06658	1.2105	0.08493	1.28458	1.2105	0.08493	1.28458	1.2105	0.08493	1.28458	0.08875	
	30	1.15126	0.03144	1.08925	0.04362	1.05333	0.05965	1.0606	0.05556	1.21497	0.06688	1.23594	1.21497	0.06688	1.23594	1.21497	0.06688	1.23594	0.05361	
	50	1.13297	0.01695	1.09885	0.02465	1.03938	0.03946	1.05172	0.03807	1.19164	0.03921	1.18718	1.19164	0.03921	1.18718	1.19164	0.03921	1.18718	0.02492	
100	1.12821	0.00762	1.12154	0.01406	1.04692	0.02906	1.05964	0.0289	1.18909	0.0257	1.16006	1.18909	0.0257	1.16006	1.18909	0.0257	1.16006	0.00991		
$S'_{pk}=0.98703$ $k=7.5$ $\zeta=1.75$	20	1.02856	0.0561	0.94299	0.04519	0.92908	0.05672	0.93065	0.05082	1.07033	0.06495	1.1319	1.07033	0.06495	1.1319	1.07033	0.06495	1.1319	0.07127	
	30	1.01381	0.02207	0.96256	0.03077	0.93504	0.04231	0.93584	0.03891	1.06941	0.04744	1.08659	1.06941	0.04744	1.08659	1.06941	0.04744	1.08659	0.03833	
	50	1.00174	0.01399	0.97554	0.01855	0.92764	0.03084	0.93518	0.02915	1.05831	0.03154	1.05072	1.05831	0.03154	1.05072	1.05831	0.03154	1.05072	0.02104	
100	0.99934	0.00633	0.99583	0.01165	0.9568	0.02195	0.94477	0.02194	1.05638	0.02263	1.02734	1.05638	0.02263	1.02734	1.05638	0.02263	1.02734	0.00842		
$\omega = 1$	$S'_{pk}=1.48556$ $k=6.5$ $\zeta=1.25$	20	1.54139	0.06236	1.42627	0.08019	1.47147	0.09572	1.42094	0.08414	1.55618	0.08735	1.69591	1.55618	0.08735	1.69591	1.55618	0.08735	1.69591	0.11878
		30	1.52667	0.0411	1.44099	0.05113	1.45854	0.08239	1.41882	0.06862	1.55539	0.06396	1.64056	1.55539	0.06396	1.64056	1.55539	0.06396	1.64056	0.06983
		50	1.51413	0.02351	1.4684	0.03287	1.46736	0.05831	1.42706	0.04925	1.56253	0.0432	1.59114	1.56253	0.0432	1.59114	1.56253	0.0432	1.59114	0.03457
	100	1.51023	0.01106	1.49936	0.01771	1.47763	0.04416	1.43954	0.03594	1.56744	0.0292	1.55541	1.56744	0.0292	1.55541	1.56744	0.0292	1.55541	0.01486	
	$S'_{pk}=1.26491$ $k=6.5$ $\zeta=1.50$	20	1.29643	0.04233	1.20125	0.05452	1.22541	0.06688	1.18827	0.06145	1.31711	0.06199	1.43435	1.31711	0.06199	1.43435	1.31711	0.06199	1.43435	0.08622
		30	1.29546	0.02956	1.22941	0.04057	1.23985	0.05689	1.20392	0.05138	1.33153	0.05125	1.39652	1.33153	0.05125	1.39652	1.33153	0.05125	1.39652	0.05171
		50	1.29237	0.0164	1.25428	0.02257	1.23972	0.04062	1.21166	0.03256	1.33481	0.03256	1.36072	1.33481	0.03256	1.36072	1.33481	0.03256	1.36072	0.02605
	100	1.281	0.00753	1.27715	0.01201	1.24399	0.02875	1.21991	0.02556	1.33618	0.02556	1.32075	1.33618	0.02556	1.32075	1.33618	0.02556	1.32075	0.01104	
	$S'_{pk}=1.09888$ $k=6.5$ $\zeta=1.75$	20	1.11731	0.03055	1.03241	0.043	1.04352	0.05404	1.0175	0.05026	1.13383	0.04727	1.23852	1.13383	0.04727	1.23852	1.13383	0.04727	1.23852	0.05837
30		1.12228	0.02119	1.07021	0.0275	1.06828	0.04013	1.04165	0.03699	1.15774	0.03597	1.21266	1.15774	0.03597	1.21266	1.15774	0.03597	1.21266	0.03925	
50		1.11932	0.01315	1.10169	0.018	1.0851	0.03482	1.05733	0.02832	1.17056	0.02757	1.17991	1.17056	0.02757	1.17991	1.17056	0.02757	1.17991	0.02078	
100	1.10738	0.00601	1.10289	0.00978	1.07507	0.02204	1.05395	0.02014	1.1568	0.01623	1.14214	1.1568	0.01623	1.14214	1.1568	0.01623	1.14214	0.00794		
$S'_{pk}=1.29514$ $k=7.5$ $\zeta=1.25$	20	1.32608	0.07087	1.20482	0.08855	1.18578	0.10199	1.1956	0.0951	1.37427	0.11544	1.44935	1.37427	0.11544	1.44935	1.37427	0.11544	1.44935	0.12568	
	30	1.30185	0.0418	1.21902	0.06	1.186	0.07443	1.19691	0.07197	1.36705	0.08177	1.3894	1.36705	0.08177	1.3894	1.36705	0.08177	1.3894	0.06607	
	50	1.29009	0.02224	1.24581	0.03845	1.19514	0.05248	1.21004	0.05255	1.36564	0.0573	1.34705	1.36564	0.0573	1.34705	1.36564	0.0573	1.34705	0.03075	
100	1.2913	0.01271	1.28035	0.02177	1.2012	0.03874	1.21781	0.03905	1.36199	0.03807	1.32559	1.36199	0.03807	1.32559	1.36199	0.03807	1.32559	0.01646		
$S'_{pk}=1.11905$ $k=7.5$ $\zeta=1.50$	20	1.13742	0.05005	1.03606	0.0659	1.02036	0.07682	1.02583	0.07232	1.18146	0.08512	1.2483	1.18146	0.08512	1.2483	1.18146	0.08512	1.2483	0.09114	
	30	1.12559	0.03479	1.05665	0.04833	1.01894	0.06295	1.028	0.06048	1.17779	0.06642	1.20342	1.17779	0.06642	1.20342	1.17779	0.06642	1.20342	0.05291	
	50	1.13057	0.01937	1.0986	0.02801	1.0986	0.02801	1.0986	0.02801	1.19726	0.02786	1.18268	1.19726	0.02786	1.18268	1.19726	0.02786	1.18268	0.02786	
100	1.11861	0.00816	1.11822	0.01581	1.05543	0.02749	1.06537	0.02749	1.19019	0.02928	1.14879	1.19019	0.02928	1.14879	1.19019	0.02928	1.14879	0.01104		
$S'_{pk}=0.98703$ $k=7.5$ $\zeta=1.75$	20	1.00616	0.03804	0.91884	0.0464	0.90215	0.05522	0.90885	0.05247	1.04566	0.06109	1.10816	1.04566	0.06109	1.10816	1.04566	0.06109	1.10816	0.07216	
	30	0.99718	0.02348	0.94917	0.03271	0.91957	0.04554	0.94273	0.05006	1.06448	0.04917	1.06448								

Table 4: Estimates and MSE for $\omega = (5, 10)$ using MLE, LSE, WLSE, PE, CME, and MPSE with S''_{pk} .

PCI	MLE			LSE			WLSE			PE			CME			MPSE		
	Parameters	S''_{pk}	n	MLE	MSE	LSE	MSE	WLSE	MSE	PE	MSE	CME	MSE	MPSE	MSE			
$\omega = 5$																		
$S''_{pk}=1.48556$ $k=6.5$ $\zeta=1.25$	20	1.59324	0.06026	1.46702	0.08273	1.45189	0.09192	1.45845	0.08885	1.62362	0.09496	1.62362	0.09496	1.76865	0.12926			
	30	1.58533	0.04587	1.49351	0.04484	1.3176	0.13923	1.47684	0.07548	1.63622	0.08389	1.63622	0.08389	1.70984	0.08222			
	50	1.56487	0.02289	1.51782	0.03526	1.2828	0.13729	1.47765	0.05047	1.63121	0.05149	1.63121	0.05149	1.64732	0.03721			
$S''_{pk}=1.26491$ $k=6.5$ $\zeta=1.50$	20	1.35465	0.04813	1.24884	0.06066	1.06366	0.08883	1.23489	0.06659	1.38294	0.07671	1.38294	0.07671	1.50611	0.10412			
	30	1.32116	0.02887	1.24935	0.03892	1.2882	0.05588	1.2223	0.05205	1.36933	0.04977	1.36933	0.04977	1.42866	0.05218			
	50	1.31847	0.0176	1.28468	0.02688	1.2937	0.05042	1.2307	0.04337	1.37572	0.04162	1.37572	0.04162	1.39303	0.02918			
$S''_{pk}=1.09888$ $k=6.5$ $\zeta=1.75$	20	1.15947	0.03488	1.07904	0.04338	1.16182	0.06879	1.06661	0.04903	1.19991	0.05793	1.19991	0.05793	1.28996	0.07506			
	30	1.14241	0.02383	1.08558	0.02879	1.15953	0.06176	1.05801	0.04027	1.18532	0.03975	1.18532	0.03975	1.25683	0.04278			
	50	1.14095	0.01333	1.11131	0.01982	1.16947	0.05451	1.06784	0.03084	1.196	0.03095	1.196	0.03095	1.20479	0.02226			
$S''_{pk}=1.29514$ $k=7.5$ $\zeta=1.25$	20	1.1582	0.12618	1.03867	0.15858	0.9794	0.20195	1.02848	0.16505	1.21419	0.17051	1.21419	0.17051	1.2465	0.18054			
	30	1.16385	0.08842	1.07561	0.10884	1.01181	0.14251	1.05677	0.1207	1.23377	0.12717	1.23377	0.12717	1.11584	0.09073			
	50	1.15853	0.05114	1.11895	0.07458	1.02441	0.10924	1.06961	0.09736	1.23899	0.09529	1.23899	0.09529	1.20199	0.06148			
$S''_{pk}=1.11905$ $k=7.5$ $\zeta=1.50$	20	1.00723	0.11626	0.90104	0.14595	0.8186	0.2092	0.8889	0.15349	1.06276	0.15405	1.06276	0.15405	1.09218	0.16447			
	30	1.00357	0.07264	0.93174	0.09543	0.83074	0.15439	0.90196	0.11314	1.06513	0.10318	1.06513	0.10318	1.0618	0.09073			
	50	1.01948	0.04	0.99133	0.05911	0.87071	0.10286	0.94007	0.0768	1.09401	0.06923	1.09401	0.06923	1.06024	0.0477			
$S''_{pk}=0.98703$ $k=7.5$ $\zeta=1.75$	20	0.89896	0.08857	0.7997	0.11611	0.70573	0.19855	0.77518	0.12914	0.93626	0.11598	0.93626	0.11598	0.96694	0.11941			
	30	0.9017	0.05798	0.83901	0.07308	0.72887	0.14564	0.80845	0.06895	0.95826	0.07643	0.95826	0.07643	0.95628	0.07442			
	50	0.90131	0.03197	0.87699	0.04407	0.76338	0.10699	0.8323	0.0614	0.96934	0.05151	0.96934	0.05151	0.93736	0.037			
$S''_{pk}=1.48556$ $k=6.5$ $\zeta=1.25$	20	1.61498	0.06574	1.4898	0.09286	1.51911	0.09226	1.48008	0.10055	1.67702	0.07352	1.67702	0.07352	1.80093	0.14361			
	30	1.59903	0.04237	1.49328	0.06347	1.5007	0.07451	1.46878	0.07623	1.686	0.05144	1.686	0.05144	1.7327	0.08006			
	50	1.58983	0.02417	1.53368	0.03692	1.51779	0.06088	1.48349	0.05795	1.68242	0.04295	1.68242	0.04295	1.6795	0.04089			
$S''_{pk}=1.26491$ $k=6.5$ $\zeta=1.50$	20	1.36396	0.05491	1.24816	0.07341	1.29292	0.0895	1.2329	0.08237	1.53892	0.09034	1.53892	0.09034	1.5301	0.12427			
	30	1.34239	0.03004	1.27162	0.04365	1.30462	0.06471	1.24255	0.05828	1.57186	0.08733	1.57186	0.08733	1.4553	0.05651			
	50	1.33814	0.01802	1.29649	0.02545	1.30354	0.04873	1.24627	0.04151	1.58511	0.08536	1.58511	0.08536	1.41341	0.03072			
$S''_{pk}=1.09888$ $k=6.5$ $\zeta=1.75$	20	1.16441	0.03786	1.07051	0.0515	1.13796	0.09465	1.05227	0.06094	1.47814	0.14919	1.47814	0.14919	1.30302	0.08319			
	30	1.14457	0.02196	1.08811	0.03356	1.16327	0.07696	1.05719	0.04608	1.19369	0.04522	1.19369	0.04522	1.24188	0.04032			
	50	1.14451	0.01354	1.12093	0.01925	1.18335	0.06687	1.09993	0.03426	1.20186	0.03233	1.20186	0.03233	1.21006	0.02236			
$S''_{pk}=1.29514$ $k=7.5$ $\zeta=1.25$	20	0.87835	0.26348	0.74793	0.28032	0.66193	0.32228	0.73349	0.28881	0.97904	0.36532	0.97904	0.36532	0.94731	0.34949			
	30	0.87024	0.20383	0.77598	0.22345	0.66415	0.26205	0.74471	0.23789	0.95896	0.28386	0.95896	0.28386	0.91341	0.24731			
	50	0.8743	0.15817	0.82733	0.17654	0.69242	0.20741	0.78167	0.19107	0.96411	0.22629	0.96411	0.22629	0.8988	0.17901			
$S''_{pk}=1.11905$ $k=7.5$ $\zeta=1.50$	20	0.75027	0.22186	0.64376	0.24586	0.49482	0.32284	0.62671	0.2554	0.81894	0.26252	0.81894	0.26252	0.8101	0.28193			
	30	0.76837	0.16898	0.70173	0.19073	0.52002	0.26983	0.66731	0.20668	0.85371	0.21299	0.85371	0.21299	0.80589	0.19884			
	50	0.78091	0.1282	0.75279	0.14587	0.54739	0.21987	0.70099	0.16708	0.87223	0.17055	0.87223	0.17055	0.80457	0.14313			
$S''_{pk}=0.98703$ $k=7.5$ $\zeta=1.75$	20	0.69021	0.18864	0.59243	0.20125	0.51141	0.24028	0.57176	0.21262	0.75118	0.2088	0.75118	0.2088	0.74778	0.23758			
	30	0.7078	0.14774	0.63559	0.16988	0.52561	0.22064	0.5968	0.19218	0.77175	0.18159	0.77175	0.18159	0.74931	0.17035			
	50	0.72775	0.10531	0.69762	0.11195	0.56043	0.16941	0.6382	0.14363	0.80784	0.13387	0.80784	0.13387	0.75284	0.11839			
$S''_{pk}=1.48556$ $k=6.5$ $\zeta=1.25$	20	1.56406	0.01076	1.53751	0.01826	1.43669	0.12458	1.46397	0.04139	1.61504	0.03919	1.61504	0.03919	1.39962	0.01495			

Table 5: Estimates of S''_{pk} , AW, and CP for ACI using MLE with $\omega = (0.01, 1, 5, 10)$.

PCI		ACI							
Parameter	n	AW	CP	AW	CP	AW	CP	AW	CP
		$\omega = 0.01$		$\omega = 1$		$\omega = 5$		$\omega = 10$	
S''_{pk}		1.48573		1.50093		1.53889		1.56048	
$\kappa=6.5$ $\zeta=1.25$	20	0.93426	0.948	0.91256	0.946	0.92149	0.943	0.95738	0.943
	30	0.75246	0.949	0.73929	0.955	0.75045	0.944	0.77221	0.957
	50	0.58055	0.957	0.56893	0.962	0.57932	0.956	0.59191	0.959
	100	0.40919	0.961	0.40182	0.964	0.40423	0.961	0.41613	0.963
S''_{pk}		1.26502		1.27436		1.29734		1.31021	
$\kappa=6.5$ $\zeta=1.50$	20	0.80269	0.949	0.78449	0.933	0.79416	0.943	0.80985	0.942
	30	0.65378	0.953	0.64050	0.945	0.64471	0.941	0.66070	0.945
	50	0.50052	0.957	0.49191	0.951	0.49220	0.956	0.50511	0.952
	100	0.35038	0.962	0.34582	0.959	0.34814	0.959	0.35444	0.953
S''_{pk}		1.09895		1.10501		1.11995		1.12819	
$\kappa=6.5$ $\zeta=1.75$	20	0.70423	0.942	0.69684	0.941	0.70924	0.938	0.74602	0.942
	30	0.570053	0.945	0.55931	0.944	0.56555	0.941	0.57962	0.947
	50	0.43880	0.949	0.43302	0.951	0.43177	0.948	0.43938	0.950
	100	0.30605	0.95	0.30274	0.953	0.30265	0.953	0.30798	0.955
S''_{pk}		1.29501		1.27988		1.17186		0.86982	
$\kappa=7.5$ $\zeta=1.25$	20	0.90836	0.937	0.93838	0.940	1.34251	0.917	1.87011	0.746
	30	0.73317	0.941	0.76631	0.943	1.11147	0.919	1.70115	0.769
	50	0.56096	0.948	0.59405	0.947	0.88337	0.933	1.43707	0.805
	100	0.39808	0.951	0.41617	0.951	0.63742	0.941	1.13160	0.868
S''_{pk}		1.11897		1.10964		1.04003		0.81598	
$\kappa=7.5$ $\zeta=1.50$	20	0.77505	0.946	0.81823	0.934	1.16887	0.918	1.72788	0.729
	30	0.63075	0.949	0.66029	0.941	0.99399	0.926	1.54389	0.736
	50	0.48786	0.953	0.51171	0.949	0.76979	0.938	1.29780	0.777
	100	0.34420	0.955	0.36017	0.952	0.55928	0.950	1.05467	0.828
S''_{pk}		0.98698		0.98084		0.93358		0.76429	
$\kappa=7.5$ $\zeta=1.75$	20	0.68964	0.929	0.71578	0.940	1.07325	0.910	1.50443	0.720
	30	0.55773	0.942	0.58301	0.947	0.90575	0.931	1.41512	0.741
	50	0.42885	0.949	0.44916	0.949	0.70608	0.943	1.22068	0.782
	100	0.30382	0.953	0.31620	0.951	0.49292	0.950	1.00100	0.841

Table 6: Estimates of $S''_{pk}(\omega)$, S'_{pk} and S_{pk} along with ABE, AW, PR and CP for $S''_{pk}(\omega)$ with, $\omega = (0.01, 1)$.

n	$\omega = 0.01$						$\omega = 1$					
	SELF	WSELF	MSELF	LLF	KLF	AW	SELF	WSELF	MSELF	LLF	KLF	AW
	ABE PR	ABE PR	ABE PR	ABE PR	ABE PR	CP	ABE PR	ABE PR	ABE PR	ABE PR	ABE PR	CP
	$\kappa=6.5$	$\zeta=1.25$	$S_{pk}=1.6000$	$S'_{pk}=1.4855$	$S''_{pk}(0.01)=1.4857$	$S''_{pk}(1)=1.5009$						
20	1.4808	1.4477	1.4146	1.4643	1.4642	0.8539	1.5069	1.4762	1.4454	1.4916	1.4915	0.8319
30	0.0494	0.0330	0.0230	0.0228	0.0230	0.9440	0.0467	0.0307	0.0210	0.0207	0.0209	0.9330
50	1.4791	1.4562	1.4333	1.4677	1.4676	0.7124	1.5080	1.4866	1.4651	1.4973	1.4972	0.6970
100	0.0341	0.0229	0.0158	0.0157	0.0158	0.9520	0.0325	0.0214	0.0145	0.0143	0.0145	0.9430
20	1.4781	1.4640	1.4499	1.4711	1.4711	0.5599	1.5067	1.4934	1.4801	1.5001	1.5000	0.5496
30	0.0208	0.0141	0.0097	0.0096	0.0097	0.9550	0.0200	0.0133	0.0089	0.0089	0.0089	0.9450
50	1.4821	1.4749	1.4677	1.4785	1.4785	0.4009	1.4988	1.4920	1.4853	1.4954	1.4954	0.3925
100	0.0106	0.0072	0.0049	0.0049	0.0049	0.9620	0.0102	0.0068	0.0046	0.0045	0.0045	0.9490
	$\kappa=6.5$	$\zeta=1.50$	$S_{pk}=1.3333$	$S'_{pk}=1.2649$	$S''_{pk}(0.01)=1.2650$	$S''_{pk}(1)=1.2744$						
20	1.2677	1.2386	1.2095	1.2532	1.2531	0.7416	1.3101	1.2826	1.2549	1.2964	1.2963	0.7343
30	0.0373	0.0291	0.0237	0.0234	0.0236	0.9490	0.0365	0.0275	0.0217	0.0213	0.0216	0.9530
50	1.2669	1.2469	1.2269	1.2569	1.2569	0.6158	1.2978	1.2791	1.2603	1.2885	1.2884	0.6042
100	0.0255	0.0200	0.0162	0.0160	0.0161	0.9490	0.0245	0.0187	0.0147	0.0146	0.0147	0.9520
20	1.2709	1.2586	1.2463	1.2648	1.2647	0.4841	1.2846	1.2730	1.2614	1.2788	1.2788	0.4743
30	0.0156	0.0122	0.0098	0.0097	0.0098	0.9540	0.0149	0.0116	0.0092	0.0091	0.0091	0.9550
50	1.2627	1.2565	1.2503	1.2596	1.2596	0.3441	1.2748	1.2689	1.2630	1.2719	1.2719	0.3386
100	0.0078	0.0062	0.0050	0.0049	0.0049	0.9600	0.0076	0.0059	0.0047	0.0047	0.0047	0.9560
	$\kappa=6.5$	$\zeta=1.75$	$S_{pk}=1.1428$	$S'_{pk}=1.0988$	$S''_{pk}(0.01)=1.0989$	$S''_{pk}(1)=1.1051$						
20	1.1024	1.0763	1.0500	1.0894	1.0893	0.6546	1.1235	1.0987	1.0737	1.1111	1.1110	0.6452
30	0.0292	0.0261	0.0245	0.0241	0.0244	0.9450	0.0282	0.0248	0.0228	0.0224	0.0226	0.9500
50	1.0994	1.0816	1.0637	1.0905	1.0905	0.5418	1.1198	1.1028	1.0858	1.1113	1.1113	0.5334
100	0.0198	0.0178	0.0166	0.0164	0.0166	0.9480	0.0191	0.0169	0.0155	0.0153	0.0154	0.9520
20	1.0916	1.0808	1.0700	1.0862	1.0862	0.4214	1.1086	1.0984	1.0880	1.1035	1.1035	0.4148
30	0.0118	0.0108	0.0101	0.0100	0.0100	0.9540	0.0114	0.0103	0.0094	0.0093	0.0094	0.9440
50	1.0960	1.0905	1.0851	1.0933	1.0933	0.3006	1.1067	1.1015	1.0962	1.1041	1.1041	0.2966
100	0.0060	0.0054	0.0050	0.0050	0.0050	0.9540	0.0058	0.0052	0.0048	0.0047	0.0048	0.9590
	$\kappa=7.5$	$\zeta=1.25$	$S_{pk}=1.3870$	$S'_{pk}=1.2951$	$S''_{pk}(0.01)=1.2950$	$S''_{pk}(1)=1.2799$						
20	1.3330	1.2984	1.2641	1.3157	1.3156	0.8286	1.3585	1.3193	1.2802	1.3390	1.3387	0.8859
30	0.0469	0.0345	0.0266	0.0265	0.0268	0.9480	0.0534	0.0391	0.0303	0.0298	0.0303	0.9360
50	1.3249	1.3008	1.2769	1.3129	1.3128	0.6931	1.3258	1.2986	1.2716	1.3122	1.3121	0.7336
100	0.0325	0.0241	0.0185	0.0185	0.0186	0.9510	0.0363	0.0271	0.0211	0.0210	0.0212	0.9490
20	1.3110	1.2961	1.2812	1.3036	1.3035	0.5454	1.3126	1.2958	1.2789	1.3042	1.3042	0.5778
30	0.0199	0.0150	0.0115	0.0115	0.0116	0.9450	0.0223	0.0169	0.0131	0.0130	0.0131	0.9530
50	1.3073	1.2996	1.2919	1.3035	1.3035	0.3921	1.2901	1.2814	1.2728	1.2857	1.2857	0.4110
100	0.0102	0.0077	0.0059	0.0059	0.0060	0.9450	0.0112	0.0086	0.0067	0.0067	0.0068	0.9590
	$\kappa=7.5$	$\zeta=1.50$	$S_{pk}=1.1735$	$S'_{pk}=1.1190$	$S''_{pk}(0.01)=1.1189$	$S''_{pk}(1)=1.1096$						
20	1.1612	1.1310	1.1010	1.1461	1.1460	0.7231	1.1848	1.1507	1.1164	1.1678	1.1676	0.7716
30	0.0358	0.0302	0.0268	0.0266	0.0269	0.9480	0.0405	0.0341	0.0305	0.0299	0.0303	0.9360
50	1.1573	1.1363	1.1155	1.1468	1.1468	0.6027	1.1587	1.1355	1.1121	1.1471	1.1470	0.6336
100	0.0246	0.0209	0.0184	0.0184	0.0185	0.9530	0.0270	0.0233	0.0209	0.0206	0.0209	0.9410
20	1.1424	1.1295	1.1166	1.1359	1.1359	0.4729	1.1302	1.1157	1.1012	1.1230	1.1229	0.4961
30	0.0149	0.0129	0.0115	0.0114	0.0115	0.9590	0.0164	0.0145	0.0131	0.0130	0.0131	0.9410
50	1.1302	1.1235	1.1169	1.1269	1.1269	0.3389	1.1256	1.1182	1.1108	1.1219	1.1219	0.3553
100	0.0076	0.0067	0.0059	0.0059	0.0060	0.9620	0.0083	0.0074	0.0067	0.0066	0.0067	0.9500
	$\kappa=7.5$	$\zeta=1.75$	$S_{pk}=1.0220$	$S'_{pk}=0.9870$	$S''_{pk}(0.01)=0.9869$	$S''_{pk}(1)=0.9808$						
20	1.0415	1.0151	0.9887	1.0283	1.0282	0.6405	1.0280	0.9985	0.9686	1.0134	1.0132	0.6673
30	0.0280	0.0265	0.0262	0.0260	0.0264	0.9370	0.0302	0.0295	0.0307	0.0299	0.0303	0.9400
50	1.0215	1.0032	0.9849	1.0123	1.0123	0.5294	1.0281	1.0076	0.9869	1.0179	1.0178	0.5594
100	0.0190	0.0183	0.0183	0.0182	0.0184	0.9390	0.0210	0.0205	0.0209	0.0205	0.0207	0.9490
20	1.0115	1.0001	0.9887	1.0058	1.0058	0.4171	0.9981	0.9855	0.9727	0.9918	0.9918	0.4356
30	0.0116	0.0114	0.0114	0.0114	0.0114	0.9430	0.0126	0.0127	0.0130	0.0129	0.0130	0.9500
50	0.9997	0.9939	0.9880	0.9968	0.9968	0.2983	0.9910	0.9845	0.9780	0.9877	0.9877	0.3111
100	0.0059	0.0059	0.0059	0.0059	0.0059	0.9480	0.0064	0.0065	0.0066	0.0066	0.0066	0.9520

Table 7: Estimates of $S''_{pk}(\omega)$, S'_{pk} and S_{pk} along with ABE, AW, PR and CP for $S''_{pk}(\omega)$ with, $\omega = (5, 10)$.

n	$\omega = 5$						$\omega = 10$					
	SELF	WSELF	MSELF	LLF	KLF	SELF	WSELF	MSELF	LLF	KLF		
	ABE PR	ABE PR	ABE PR	ABE PR	ABE PR	AW CP	ABE PR	ABE PR	ABE PR	ABE PR	ABE PR	AW CP
	$\kappa=6.5$		$\zeta=1.25$	$S_{pk}=1.6000$		$S'_{pk}=1.4856$	$S''_{pk}(5)=1.5389$		$S''_{pk}(10)=1.5605$			
20	1.5827	1.5518	1.5195	1.5675	1.5672	0.8475	1.6106	1.5714	1.4916	1.5930	1.5908	0.8892
30	0.0481	0.0309	0.0212	0.0199	0.0201	0.9370	0.0535	0.0392	0.0583	0.0243	0.0268	0.9280
50	1.5710	1.5499	1.5284	1.5605	1.5604	0.7062	1.5974	1.5743	1.5475	1.5861	1.5858	0.7322
100	0.0331	0.0212	0.0139	0.0136	0.0137	0.9460	0.0358	0.0231	0.0176	0.0146	0.0148	0.9480
	$\kappa=6.5$		$\zeta=1.50$	$S_{pk}=1.3333$		$S'_{pk}=1.2649$	$S''_{pk}(5)=1.2973$		$S''_{pk}(10)=1.3102$			
20	1.5570	1.5400	1.5308	1.5505	1.5505	0.5536	1.5789	1.5652	1.5514	1.5721	1.5720	0.5695
30	0.0203	0.0130	0.0085	0.0084	0.0085	0.9460	0.0215	0.0136	0.0088	0.0087	0.0087	0.9480
50	1.5462	1.5395	1.5328	1.5428	1.5428	0.3957	1.5683	1.5614	1.5544	1.5648	1.5648	0.4067
100	0.0103	0.0067	0.0044	0.0043	0.0043	0.9500	0.0109	0.0070	0.0045	0.0044	0.0045	0.9530
	$\kappa=6.5$		$\zeta=1.75$	$S_{pk}=1.1429$		$S'_{pk}=1.0989$	$S''_{pk}(5)=1.1199$		$S''_{pk}(10)=1.1282$			
20	1.3340	1.3049	1.2720	1.3198	1.3194	0.7446	1.3757	1.3273	1.1824	1.3572	1.3507	0.8034
30	0.0372	0.0290	0.0265	0.0223	0.0228	0.9420	0.0443	0.0484	0.1313	0.0339	0.0467	0.9460
50	1.3311	1.3121	1.2925	1.3217	1.3216	0.6139	1.3488	1.3256	1.2856	1.3381	1.3371	0.6397
100	0.0251	0.0190	0.0151	0.0144	0.0146	0.9450	0.0276	0.0232	0.0334	0.0172	0.0181	0.9510
	$\kappa=7.5$		$\zeta=1.25$	$S_{pk}=1.3870$		$S'_{pk}=1.2951$	$S''_{pk}(5)=1.1719$		$S''_{pk}(10)=0.8698$			
20	1.3112	1.2997	1.2882	1.3055	1.3054	0.4753	1.3267	1.3147	1.3022	1.3208	1.3207	0.4875
30	0.0150	0.0114	0.0089	0.0088	0.0088	0.9490	0.0158	0.0120	0.0096	0.0091	0.0092	0.9530
50	1.3126	1.3068	1.3009	1.3097	1.3097	0.3416	1.3227	1.3167	1.3106	1.3197	1.3197	0.3477
100	0.0077	0.0059	0.0045	0.0045	0.0045	0.9500	0.0080	0.0060	0.0046	0.0046	0.0046	0.9520
	$\kappa=7.5$		$\zeta=1.50$	$S_{pk}=1.1735$		$S'_{pk}=1.1191$	$S''_{pk}(5)=1.0400$		$S''_{pk}(10)=0.8160$			
20	1.1733	1.1448	1.1075	1.1597	1.1589	0.6743	1.1797	1.1005	0.8478	1.1572	1.1572	0.7412
30	0.0307	0.0284	0.0355	0.0289	0.0258	0.9470	0.0389	0.0792	0.2905	0.0611	0.1773	0.9350
50	1.1574	1.1401	1.1217	1.1489	1.1487	0.5434	1.1661	1.1351	1.0474	1.1541	1.1501	0.5840
100	0.0197	0.0174	0.0163	0.0152	0.0153	0.9510	0.0237	0.0310	0.0943	0.0263	0.0348	0.9410
	$\kappa=7.5$		$\zeta=1.75$	$S_{pk}=1.0220$		$S'_{pk}=0.9870$	$S''_{pk}(5)=0.9336$		$S''_{pk}(10)=0.7643$			
20	1.1375	1.1273	1.1170	1.1324	1.1324	0.4181	1.1512	1.1399	1.1265	1.1457	1.1455	0.4306
30	0.0116	0.0102	0.0092	0.0090	0.0091	0.9510	0.0124	0.0113	0.0121	0.0099	0.0100	0.9420
50	1.1326	1.1275	1.1223	1.1301	1.1300	0.2980	1.1371	1.1318	1.1264	1.1345	1.1345	0.3021
100	0.0059	0.0052	0.0046	0.0046	0.0046	0.9530	0.0060	0.0053	0.0047	0.0047	0.0047	0.9450
	$\kappa=7.5$		$\zeta=1.25$	$S_{pk}=1.0220$		$S'_{pk}=0.9870$	$S''_{pk}(5)=0.9336$		$S''_{pk}(10)=0.7643$			
20	1.2169	1.1157	0.9773	1.1712	1.1646	1.1543	1.0234	0.6668	0.2546	0.8868	0.8118	1.4698
30	0.0903	0.1011	0.1526	0.1021	0.1138	0.9330	0.1750	0.3566	0.7657	0.5990	1.3627	0.8920
50	1.2036	1.1335	1.0474	1.1709	1.1678	1.0003	0.9780	0.7168	0.3920	0.8693	0.8305	1.3380
100	0.0672	0.0701	0.0877	0.0678	0.0720	0.9430	0.1430	0.2612	0.5781	0.4236	0.6598	0.8990
	$\kappa=7.5$		$\zeta=1.50$	$S_{pk}=1.1735$		$S'_{pk}=1.1191$	$S''_{pk}(5)=1.0400$		$S''_{pk}(10)=0.8160$			
20	1.1787	1.1341	1.0836	1.1574	1.1561	0.8173	0.9391	0.7628	0.5421	0.8614	0.8440	1.1788
30	0.0447	0.0445	0.0491	0.0420	0.0434	0.9440	0.1076	0.1763	0.3605	0.2685	0.3406	0.9150
50	1.1761	1.1534	1.1291	1.1650	1.1647	0.6039	0.8995	0.7974	0.6780	0.8521	0.8464	0.9773
100	0.0243	0.0227	0.0224	0.0206	0.0209	0.9500	0.0704	0.1022	0.1750	0.1421	0.1575	0.9280
	$\kappa=7.5$		$\zeta=1.75$	$S_{pk}=1.0220$		$S'_{pk}=0.9870$	$S''_{pk}(5)=0.9336$		$S''_{pk}(10)=0.7643$			
20	1.0664	0.9592	0.7996	1.0195	1.0104	1.0623	0.8622	0.5007	0.1600	0.7235	0.6356	1.2980
30	0.0777	0.1072	0.2121	0.1291	0.1508	0.9190	0.1444	0.3615	0.8417	0.8542	2.8453	0.8990
50	1.0408	0.9660	0.8677	1.0067	1.0023	0.9161	0.8465	0.5734	0.2502	0.7366	0.6869	1.1938
100	0.0573	0.0748	0.1237	0.0877	0.0958	0.9350	0.1186	0.2730	0.6997	0.5653	1.0768	0.9070
	$\kappa=7.5$		$\zeta=1.75$	$S_{pk}=1.0220$		$S'_{pk}=0.9870$	$S''_{pk}(5)=0.9336$		$S''_{pk}(10)=0.7643$			
20	1.0398	0.9970	0.9458	1.0197	1.0181	0.7256	0.8231	0.6359	0.3989	0.7429	0.7196	1.0627
30	0.0357	0.0428	0.0587	0.0472	0.0493	0.9400	0.0908	0.1872	0.4701	0.3488	0.4870	0.9200
50	1.0296	1.0082	0.9847	1.0192	1.0188	0.5334	0.8234	0.7174	0.5834	0.7759	0.7677	0.8787
100	0.0192	0.0214	0.0252	0.0225	0.0229	0.9440	0.0592	0.1060	0.2262	0.1695	0.1960	0.9310
	$\kappa=7.5$		$\zeta=1.75$	$S_{pk}=1.0220$		$S'_{pk}=0.9870$	$S''_{pk}(5)=0.9336$		$S''_{pk}(10)=0.7643$			
20	0.9361	0.8223	0.6372	0.8884	0.8758	0.9646	0.7851	0.3963	0.1050	0.6467	0.5265	1.1588
30	0.0651	0.1138	0.2958	0.1644	0.2076	0.9210	0.1188	0.3888	0.8942	1.0364	9.5793	0.8990
50	0.9319	0.8580	0.7520	0.8993	0.8936	0.8175	0.7538	0.4661	0.1662	0.6429	0.5775	1.0583
100	0.0464	0.0738	0.1575	0.1013	0.1151	0.9320	0.0976	0.2876	0.7962	0.7318	1.9367	0.9080
	$\kappa=7.5$		$\zeta=1.75$	$S_{pk}=1.0220$		$S'_{pk}=0.9870$	$S''_{pk}(5)=0.9336$		$S''_{pk}(10)=0.7643$			
20	0.9174	0.8739	0.8180	0.8975	0.8953	0.6587	0.7382	0.5429	0.2950	0.6580	0.6272	0.9460
30	0.0298	0.0435	0.0753	0.0556	0.0590	0.9460	0.0752	0.1953	0.5815	0.4408	0.7137	0.9050
50	0.9138	0.8935	0.8702	0.9041	0.9035	0.4750	0.7466	0.6357	0.4900	0.6982	0.6874	0.7962
100	0.0155	0.0203	0.0290	0.0248	0.0253	0.9500	0.0507	0.1109	0.2904	0.2091	0.2563	0.9180

4. APPLICATIONS

This section deals with the real life application of the considered study. Considering two real data sets one is for aluminium foil and other is for liquid crystal display, before including there data sets in our study we use "R programming" for goodness of fit test, in particular use *fitdistrplus* Delignette-Muller and Dutang, [5] package to get the K-S test value and *p*-value for given data sets.

Data Set I

The dataset, consisting of 50 observation, is sourced from Saha [17]; Saha and Dey [21] and records the voltage of aluminium foil used by an electronics manufacturer. The production specifications of the voltage are set as $(L, T, U) = (510, 520, 530)$. This voltage range is crucial to prevent the aluminium foil from breaking, which would lead to its rejection.

Using the *fitdistrplus* package, we firstly check for normality test and then obtained the estimated values of κ and ζ as 519.7560, 1.7658, respectively. Additionally, the one sample Kolmogorov-Smirnov statistic and its p -values are (0.0734, 0.9505), respectively, indicated a good fit.

Data Set II

The data, sourced from Peng [16]; Wu and Pearn [27] and also used by Saha and Dey [21], represents the glass substrate thickness (in *mm*) of the STN-LCD, (liquid crystal display). If the product’s characteristic falls outside this range, $\mathbb{L} = 0.63$ and $\mathbb{U} = 0.77$, with $\mathbb{T} = 0.70$ the lifetime or reliability of the STN-LCD will be deemed unacceptable and the product will be rejected. Before moving forward, we first examine whether the normal distribution is appropriate for analyzing the given dataset. For dataset II, the MLEs of κ and ζ are found to be $\hat{\kappa}_{mle} = 0.7096$, $\hat{\zeta}_{mle} = 0.0193$. The one sample (K-S statistic, p -values) are (0.0707, 0.8250), respectively. For given specifications of two data sets the classical and Bayes estimates for S''_{pk} with four different ω values are calculated. In classical setup, MLE and MPSIE are considered for providing the point and interval estimates (AIC) and are reported in Table 8. The Bayes estimates are obtained for five different loss functions along with IHPD credible intervals are also obtained and shown in Table 8. Further, the Bayes point and interval estimates of the considered PCI are computed under the assumption of non-informative priors using different loss functions for various values of $\omega = 0.01$ to 10. the values of hyper-parameters are chosen as $\alpha = (1.05, 1.55)$, $\beta = (0.01, 0.001)$ and $\kappa_0 = (520, 0.70)$, respectively. The obtained result is reported in Table 8. The mixing of the chain based on generated sequence of posterior samples under MCMC approach for both the data sets is investigate through the corresponding trace plot, which is given in Figure 1. This suggests that the generated samples are effectively mixed and converge to the true parameter values.

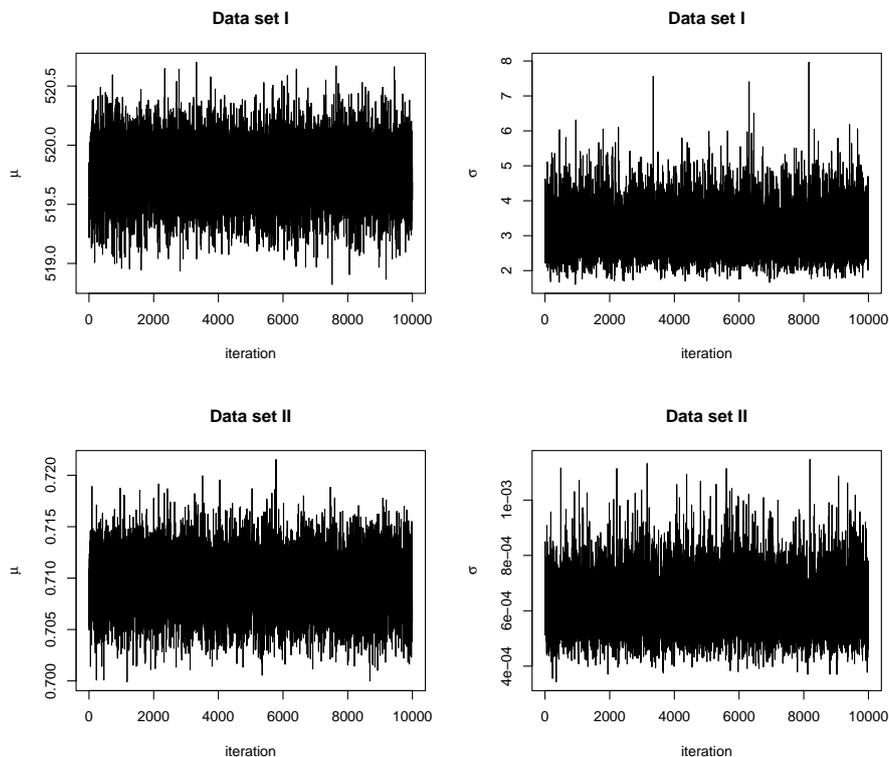


Figure 1: Trace plot for the considered real data sets I and II.

Table 8: Classical and Bayesian estimates of S''_{pk} using MLE and MPSE for real data sets with $\omega = (0.01, 1, 5, 10)$.

Point and Interval Estimates							
Data set	n	Method of Estimation	Classical Estimate	Width			
				ACI	GCI	BCI	
						P- boot	S- boot
$\omega = 0.01$							
I	50	MLE	1.8539	0.7475	0.7295	0.7399	0.7330
		MPSE	1.8359	0.7400	0.7350	0.8223	0.8154
II	79	MLE	1.0012	0.3532	0.3446	0.3656	0.3607
		MPSE	0.9966	0.3517	0.3453	0.3742	0.3745
$\omega = 1$							
I	50	MLE	1.8553	0.7440	0.7207	0.7682	0.7725
		MPSE	1.8372	0.7366	0.7464	0.8137	0.8021
II	79	MLE	1.0009	0.3535	0.3400	0.3618	0.3556
		MPSE	0.9963	0.3519	0.3441	0.3824	0.3858
$\omega = 5$							
I	50	MLE	1.8593	0.7361	0.7254	0.7578	0.7462
		MPSE	1.8411	0.7289	0.7174	0.8085	0.8032
II	79	MLE	0.9998	0.3547	0.3448	0.3785	0.3676
		MPSE	0.9952	0.3532	0.3498	0.4060	0.3954
$\omega = 10$							
I	50	MLE	1.8624	0.7327	0.7364	0.7889	0.7839
		MPSE	1.8441	0.7255	0.7497	0.7669	0.7858
II	79	MLE	0.9983	0.3563	0.3443	0.3452	0.3568
		MPSE	0.9937	0.3547	0.3516	0.4090	0.3950
Bayes Point Estimates and Credible Interval Estimates							
			BIE				Width
			SELF	WSELF	MSELF	LLF	KLF
$\omega = 0.01$							
I	50	1.8588	1.8398	1.8207	1.8493	1.8493	0.7309
II	79	0.9889	0.9811	0.9733	0.9850	0.9850	0.3403
$\omega = 1$							
I	50	1.8633	1.8445	1.8254	1.8539	1.8538	0.7291
II	79	0.9882	0.9805	0.9729	0.9843	0.9844	0.3426
$\omega = 5$							
I	50	1.8719	1.8541	1.8362	1.8631	1.8630	0.7061
II	79	0.9867	0.9789	0.9713	0.9828	0.9828	0.3382
$\omega = 10$							
I	50	1.8730	1.8532	1.8308	1.8634	1.8631	0.7149
II	79	0.9854	0.9775	0.9696	0.9814	0.9814	0.3436

5. CONCLUSIONS

In this article, the point and interval estimation have been considered under classical and Bayesian paradigm for newly proposed index S''_{pk} , when the process is normally distributed. Under classical estimation for the index, six methods were studied. One approach was explored to obtain the interval estimation: Δ CI based on MLE. In order to evaluate the effectiveness of each of these point and interval estimations, we conducted Monte Carlo simulation studies with various layouts, obtaining MSEs for point estimation and Δ Ws, CPs for interval estimation, respectively. According to the simulation studies, observed that MLE performed better in terms of their MSE for point estimation, whereas Δ CI shows appropriate pattern in terms of Δ Ws for interval estimation. The Bayes (point and interval) estimations are carried out for the index S''_{pk} with five different loss functions. The same setups were used for the Bayesian estimation. The comparison was considered with the help of average BE and corresponding PR obtained by simulation study. According to this, LLF has the lowest PR and SELF has the highest BE with decreasing Δ W and increase in CP as sample size rise. Two real data sets were re-analyzed, and the results were consistent with the findings of the considered simulation study. Real life experiment reveals that SELF has the largest BE for all four sets of ω values. For further study the present study may be extended for the censored scheme. We hope that the results obtained in this study will help the practitioners in the manufacturing industries in their decision making.

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